

```

> # Prof. Dr. Serkan Dağ
# ME 451 Introduction to Composite Structures
> # File 7.4.4
# Example on design of a laminate

> restart :
with(LinearAlgebra) :
  Digits := 24 :
> # Enter the number of plies
> n := 100 :
> # Define extensional, coupling, and bending stiffness matrices
> A := Matrix(3) :
  B := Matrix(3) :
  Dm := Matrix(3) :
> # Define laminate stiffness matrix
> QL := Matrix(6) :
> # Define ply surface coordinate vector in inches
> h := Matrix(n + 1, 1) :
> h[1, 1] := -50·0.0049213 :
  for i from 2 by 1 to n + 1
  while true do
    h[i, 1] := h[i - 1, 1] + 0.0049213 :
  end do:
> # Define ply angle vector in radians
> theta := Matrix(n, 1) :
> for i from 1 by 1 to n
  while true do
    theta[i, 1] := 0 :
  end do:
> # Define Qbar array
Qbar := Array(1..3, 1..3, 1..n) :
  ArrayNumElems(Qbar);

```

900

(1)

```

> # Enter properties of the unidirectional lamina
# From Table 2.2 for graphite/epoxy (unit = Msi)
> E1c := 26.25 :
  E2c := 1.49 :
  ν12c := 0.28 :
  G12c := 1.040 :
> # Calculate elements of the compliance matrix for the
graphite/epoxy unidirectional lamina
> S11c :=  $\frac{1}{E1_c}$  :
  S12c :=  $-\frac{\nu12_c}{E1_c}$  :

```

$$S22_c := \frac{1}{E2_c} :$$

$$S66_c := \frac{1}{G12_c} :$$

> # Calculate elements of the reduced stiffness matrix for the graphite/epoxy unidirectional lamina

$$Q11_c := \frac{S22_c}{S11_c \cdot S22_c - S12_c^2} :$$

$$Q22_c := \frac{S11_c}{S11_c \cdot S22_c - S12_c^2} :$$

$$Q12_c := -\frac{S12_c}{S11_c \cdot S22_c - S12_c^2} :$$

$$Q66_c := \frac{1}{S66_c} :$$

> # Enter properties of the unidirectional lamina
From Table 2.2 for glass/epoxy (unit = Msi)

$$E1_g := 5.6 :$$

$$E2_g := 1.2 :$$

$$\nu12_g := 0.26 :$$

$$G12_g := 0.6 :$$

> # Calculate elements of the compliance matrix for the glass/epoxy unidirectional lamina

$$S11_g := \frac{1}{E1_g} :$$

$$S12_g := -\frac{\nu12_g}{E1_g} :$$

$$S22_g := \frac{1}{E2_g} :$$

$$S66_g := \frac{1}{G12_g} :$$

> # Calculate elements of the reduced stiffness matrix for the glass/epoxy unidirectional lamina

$$Q11_g := \frac{S22_g}{S11_g \cdot S22_g - S12_g^2} :$$

$$Q22_g := \frac{S11_g}{S11_g \cdot S22_g - S12_g^2} :$$

$$Q12_g := -\frac{S12_g}{S11_g \cdot S22_g - S12_g^2} :$$

$$Q66_g := \frac{1}{S66_g} :$$

```

> # Calculate elements of transformed reduced stiffness matrix for
  # each angle lamina
  # Unit = Msi
> for i from 1 by 1 to n
  while true do
    if i < 41 or i > 60 then
      Qbar[1, 1, i] := Q11c · (cos(theta[i, 1]))4 + Q22c · (sin(theta[i, 1]))4 + 2 · (Q12c + 2 · Q66c)
        · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2 :
      Qbar[1, 2, i] := (Q11c + Q22c - 4 · Q66c) · (sin(theta[i, 1]))2 · (cos(theta[i, 1]))2 + Q12c
        · ((cos(theta[i, 1]))4 + (sin(theta[i, 1]))4) :
      Qbar[1, 3, i] := (Q11c - Q12c - 2 · Q66c) · (sin(theta[i, 1])) · (cos(theta[i, 1]))3 - (Q22c
        - Q12c - 2 · Q66c) · (sin(theta[i, 1]))3 · cos(theta[i, 1]) :
      Qbar[2, 2, i] := Q11c · (sin(theta[i, 1]))4 + Q22c · (cos(theta[i, 1]))4 + 2 · (Q12c + 2 · Q66c)
        · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2 :
      Qbar[2, 3, i] := (Q11c - Q12c - 2 · Q66c) · (cos(theta[i, 1])) · (sin(theta[i, 1]))3 - (Q22c
        - Q12c - 2 · Q66c) · (cos(theta[i, 1]))3 · sin(theta[i, 1]) :
      Qbar[3, 3, i] := (Q11c + Q22c - 2 · Q12c - 2 · Q66c) · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2
        + Q66c · ((cos(theta[i, 1]))4 + (sin(theta[i, 1]))4) :
      Qbar[2, 1, i] := Qbar[1, 2, i] :
      Qbar[3, 1, i] := Qbar[1, 3, i] :
      Qbar[3, 2, i] := Qbar[2, 3, i] :

    else

      Qbar[1, 1, i] := Q11g · (cos(theta[i, 1]))4 + Q22g · (sin(theta[i, 1]))4 + 2 · (Q12g + 2 · Q66g)
        · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2 :
      Qbar[1, 2, i] := (Q11g + Q22g - 4 · Q66g) · (sin(theta[i, 1]))2 · (cos(theta[i, 1]))2 + Q12g
        · ((cos(theta[i, 1]))4 + (sin(theta[i, 1]))4) :
      Qbar[1, 3, i] := (Q11g - Q12g - 2 · Q66g) · (sin(theta[i, 1])) · (cos(theta[i, 1]))3 - (Q22g
        - Q12g - 2 · Q66g) · (sin(theta[i, 1]))3 · cos(theta[i, 1]) :
      Qbar[2, 2, i] := Q11g · (sin(theta[i, 1]))4 + Q22g · (cos(theta[i, 1]))4 + 2 · (Q12g + 2 · Q66g)
        · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2 :
      Qbar[2, 3, i] := (Q11g - Q12g - 2 · Q66g) · (cos(theta[i, 1])) · (sin(theta[i, 1]))3 - (Q22g
        - Q12g - 2 · Q66g) · (cos(theta[i, 1]))3 · sin(theta[i, 1]) :
      Qbar[3, 3, i] := (Q11g + Q22g - 2 · Q12g - 2 · Q66g) · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2
        + Q66g · ((cos(theta[i, 1]))4 + (sin(theta[i, 1]))4) :
      Qbar[2, 1, i] := Qbar[1, 2, i] :
      Qbar[3, 1, i] := Qbar[1, 3, i] :
      Qbar[3, 2, i] := Qbar[2, 3, i] :

    end if:
  end while
end for

```

```

end do:
> # Calculate elements of extensional stiffness matrix [A],
coupling stiffness matrix [B], and bending stiffness matrix [Dm]
# Units: [A]--> Msi.in; [B]--> Msi.in^2; [Dm]--> Msi.in^3
> for i from 1 by 1 to 3
  while true do
  for j from 1 by 1 to 3
  while true do
    A[i,j]=0 :
    B[i,j] := 0 :
    Dm[i,j] := 0 :
    for k from 1 by 1 to n
    while true do
      A[i,j] := A[i,j] + Qbar[i,j,k]·(h[k+1,1] - h[k,1]) :
      B[i,j] := B[i,j] +  $\frac{1}{2}$  · Qbar[i,j,k]·(h[k+1,1]2 - h[k,1]2) :
      Dm[i,j] := Dm[i,j] +  $\frac{1}{3}$  · Qbar[i,j,k]·(h[k+1,1]3 - h[k,1]3) :
    end do:
    end do:
  end do:
> evalf( A );
[[10.9402137827591637577543, 0.196147816359409931642728, 0.], (2)
 [0.196147816359409931642728, 0.709088435095022051280866, 0.],
 [0., 0., 0.46850776000000000000000000]]
> evalf( B );

$$\begin{bmatrix} 0. & 3.1 \cdot 10^{-26} & 0. \\ 3.1 \cdot 10^{-26} & -1.3 \cdot 10^{-25} & 0. \\ 0. & 0. & 0. \end{bmatrix}$$
 (3)
> evalf( Dm );
[[0.260249774977115048492556, 0.00415421622987462298168355, 0.], (4)
 [0.00415421622987462298168355, 0.0148433974979491765231051, 0.],
 [0., 0., 0.0102948305093191382133336]]
> # Form laminate stiffness matrix QL
> for i from 1 by 1 to 3
  while true do
  for j from 1 by 1 to 3
  while true do
    QL[i,j] := A[i,j]:
    QL[i,j+3] := B[i,j]:
    QL[i+3,j] := B[i,j]:
    QL[i+3,j+3] := Dm[i,j]:
  end do:
  end do:
> # Form loading vector N

```

$$N := \begin{bmatrix} 0 \\ 0 \\ 0 \\ 3250 \cdot (10)^{-6} \\ 0 \\ 0 \end{bmatrix};$$

$$N := \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{13}{4000} \\ 0 \\ 0 \end{bmatrix}$$

(5)

> # Find midplane strains and curvatures

> Res := evalf(LinearSolve(QL, N));

$$Res := \begin{bmatrix} 3.14759693084734420145451 \cdot 10^{-29} \\ -1.20073852938493623205765 \cdot 10^{-27} \\ 0. \\ 0.0125440423255924564682719 \\ -0.00351069653860648893107346 \\ 0. \end{bmatrix}$$

(6)

> # Find strains

> eps_x := z·Res[4, 1];

eps_y := z·Res[5, 1];

$$eps_x := 0.0125440423255924564682719 z$$

$$eps_y := -0.00351069653860648893107346 z$$

(7)

> # Stresses in any of the graphite/epoxy lamina

> σ_{xc} := Qbar[1, 1, 1]·eps_x + Qbar[1, 2, 1]·eps_y;

σ_{yc} := Qbar[2, 1, 1]·eps_x + Qbar[2, 2, 1]·eps_y;

σ_{xy_c} := Qbar[3, 1, 1]·eps_x + Qbar[3, 2, 1]·eps_y;

$$\sigma_{xc} := 0.329281796348887417302078 z$$

$$\sigma_{yc} := 0.00000244750744798217835492 z$$

$$\sigma_{xy_c} := 0.$$

(8)

> # Find strength ratios at z=h[101,1]

$$\begin{aligned} &> \frac{\left(\frac{217.56}{2 \cdot 1000}\right)}{\text{subs}(z=h[101, 1], \sigma_{xc})}; \\ & \hspace{15em} 1.34255314913481870373960 \end{aligned} \tag{9}$$

$$\begin{aligned} &> \frac{\left(\frac{5.802}{2 \cdot 1000}\right)}{\text{subs}(z=h[101, 1], \sigma_{yc})}; \\ & \hspace{15em} 4816.96911968401158447657 \end{aligned} \tag{10}$$

> # Find strength ratios at z=h[1,1]

$$\begin{aligned} &> \frac{\left(\frac{-217.56}{2 \cdot 1000}\right)}{\text{subs}(z=h[1, 1], \sigma_{xc})}; \\ & \hspace{15em} 1.34255314913481870373960 \end{aligned} \tag{11}$$

$$\begin{aligned} &> \frac{\left(\frac{-35.68}{2 \cdot 1000}\right)}{\text{subs}(z=h[1, 1], \sigma_{yc})}; \\ & \hspace{15em} 29622.4505671019533495560 \end{aligned} \tag{12}$$

> # Stresses in any of the glass/epoxy lamina

$$\begin{aligned} &> \sigma_{xg} := Qbar[1, 1, 41] \cdot eps_x + Qbar[1, 2, 41] \cdot eps_y; \\ & \quad \sigma_{yg} := Qbar[2, 1, 41] \cdot eps_x + Qbar[2, 2, 41] \cdot eps_y; \\ & \quad \sigma_{xyg} := Qbar[3, 1, 41] \cdot eps_x + Qbar[3, 2, 41] \cdot eps_y; \\ & \hspace{15em} \sigma_{xg} := 0.0701677293831948107921598 z \\ & \hspace{15em} \sigma_{yg} := -0.00030349092354979011601068 z \\ & \hspace{18em} \sigma_{xyg} := 0. \end{aligned} \tag{13}$$

> # Find strength ratios at z=h[61,1]

$$\begin{aligned} &> \frac{\left(\frac{154.03}{2 \cdot 1000}\right)}{\text{subs}(z=h[61, 1], \sigma_{xg})}; \\ & \hspace{15em} 22.3027315250340074609415 \end{aligned} \tag{14}$$

$$\begin{aligned} &> \frac{\left(\frac{-17.12}{2 \cdot 1000}\right)}{\text{subs}(z=h[61, 1], \sigma_{yg})}; \\ & \hspace{15em} 573.123501135525279979067 \end{aligned} \tag{15}$$

> # Find strength ratios at z=h[41,1]

$$\begin{aligned} &> \frac{\left(\frac{-88.47}{2 \cdot 1000}\right)}{\text{subs}(z=h[41, 1], \sigma_{xg})}; \\ & \hspace{15em} 12.8099893398672897492014 \end{aligned} \tag{16}$$

```
> 
$$\frac{\left(\frac{4.496}{2 \cdot 1000}\right)}{\text{subs}(z=h[41, 1], \sigma_{yg})};$$
  
150.511872728114582873007 (17)
```

```
> # Therefore, strength ratio is 1.3426  
> # Calculate total cost  
> cost := 80·10 + 20·4;  
cost := 880 (18)  
>
```