

House Project in Ümitköy

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Group 2

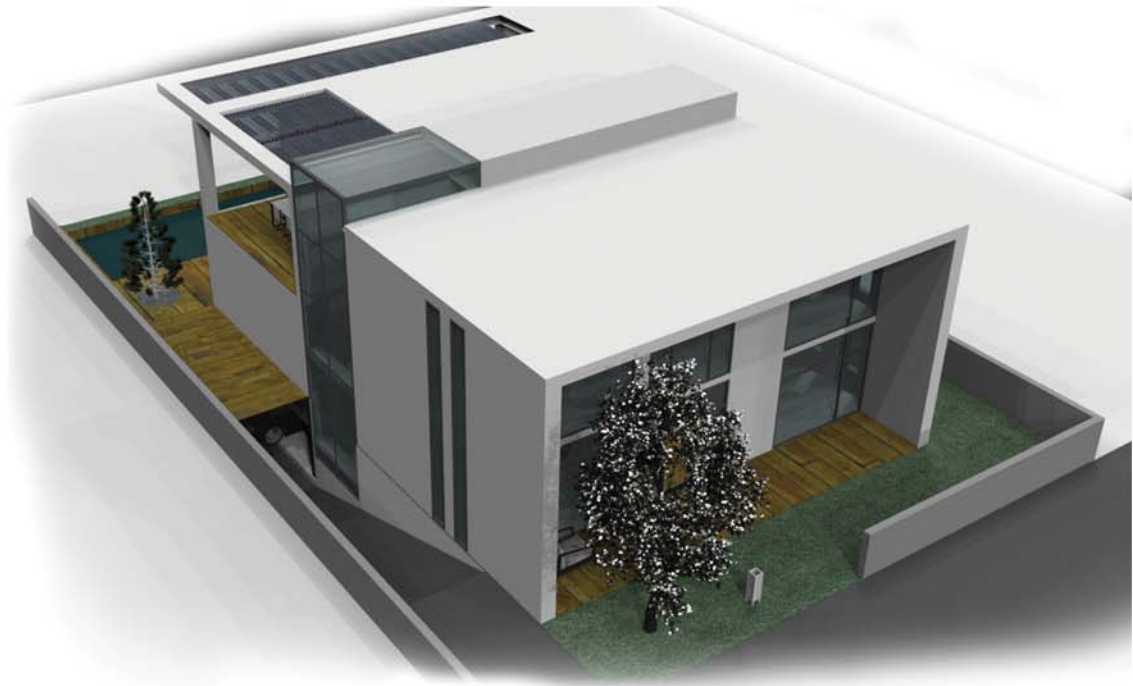
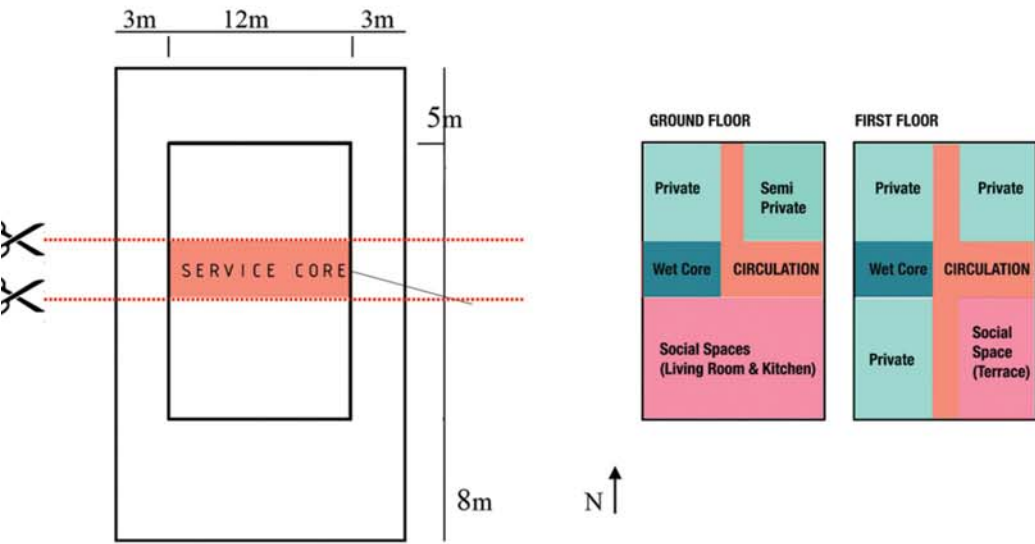
2013-14, Spring

Banu Deniz
Gökçe Altay
Demet Çekiç

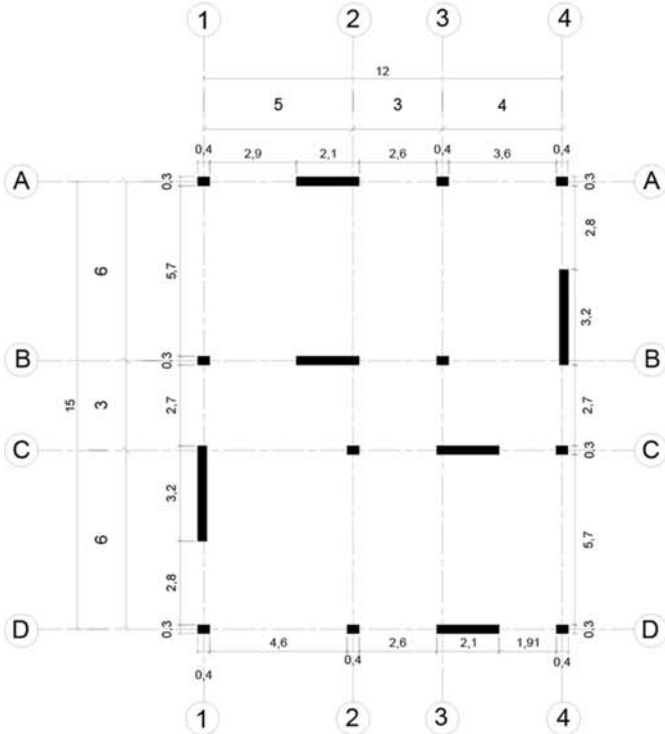


ARCH332 HOUSE Umitköy

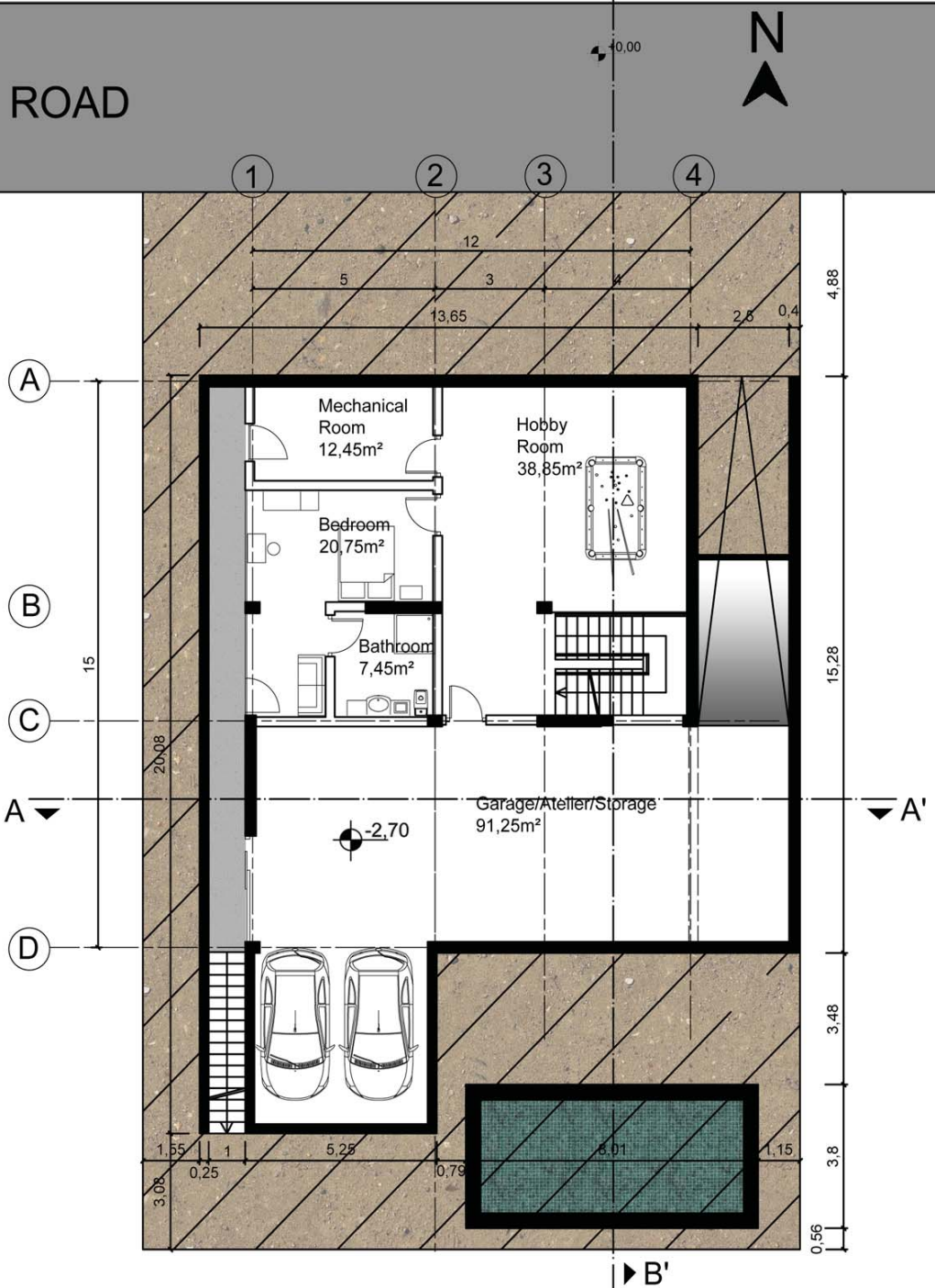
Design Idea & 3D Images



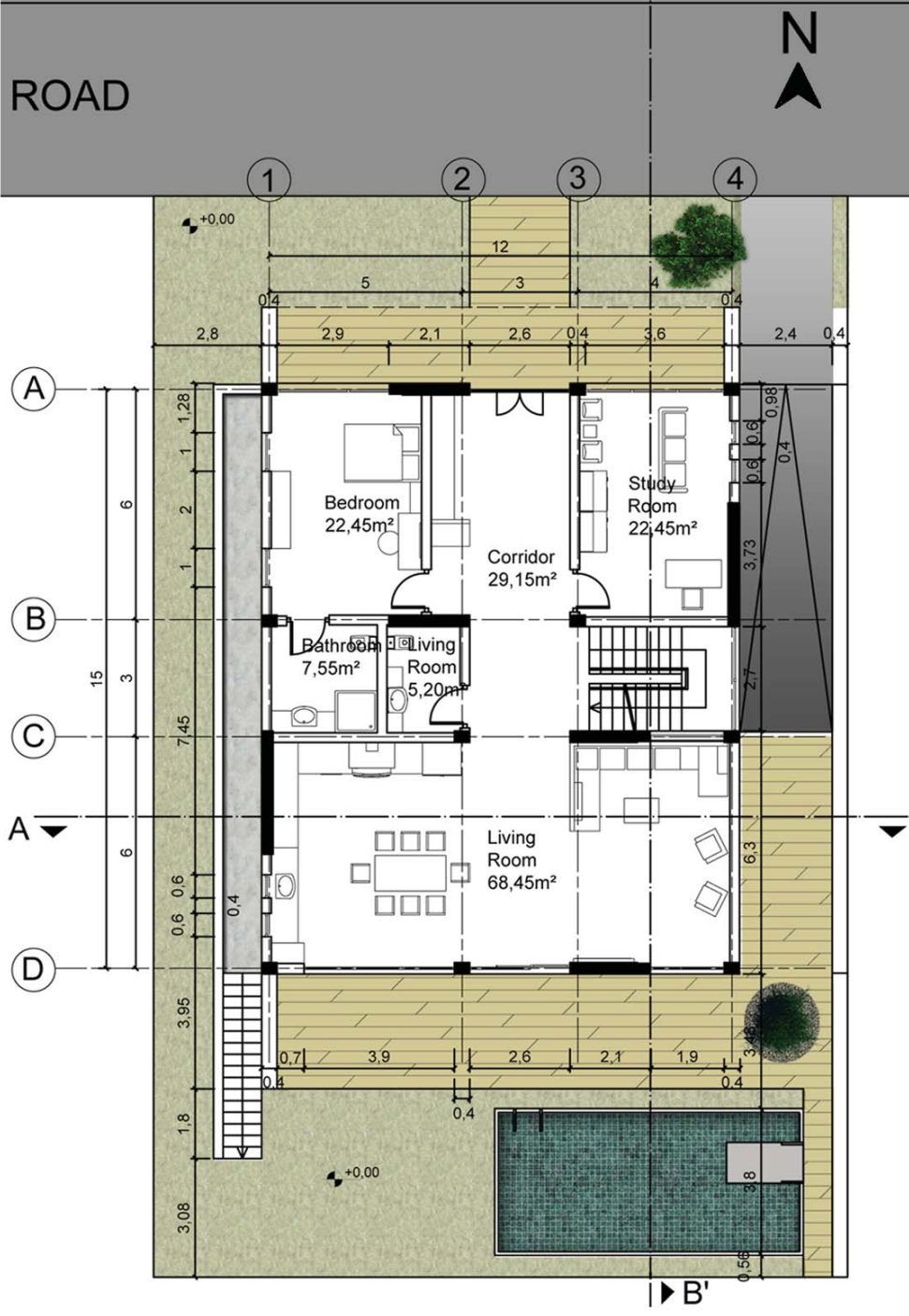
Structural System



-2.70 Floor Plan

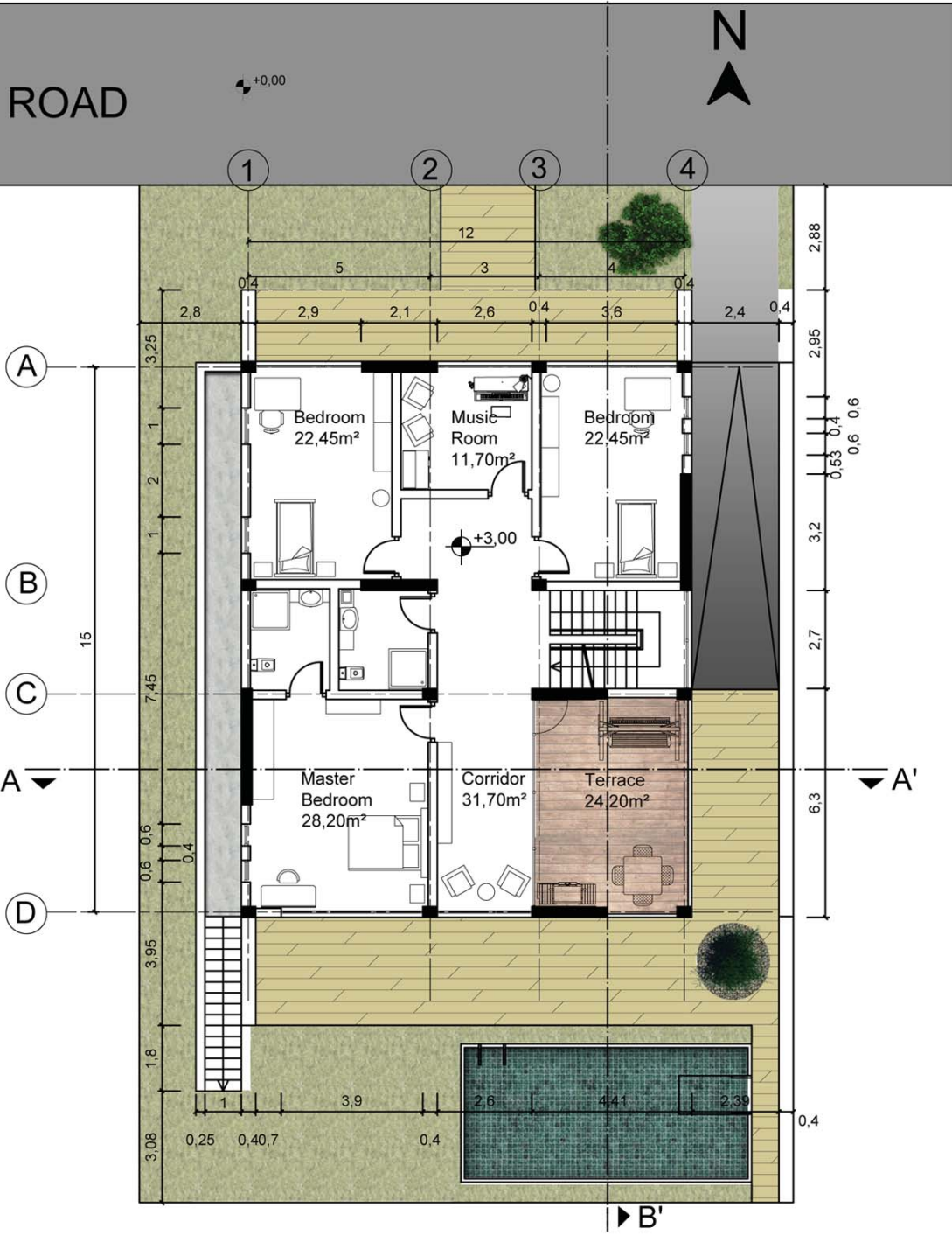


+0.00 Floor Plan

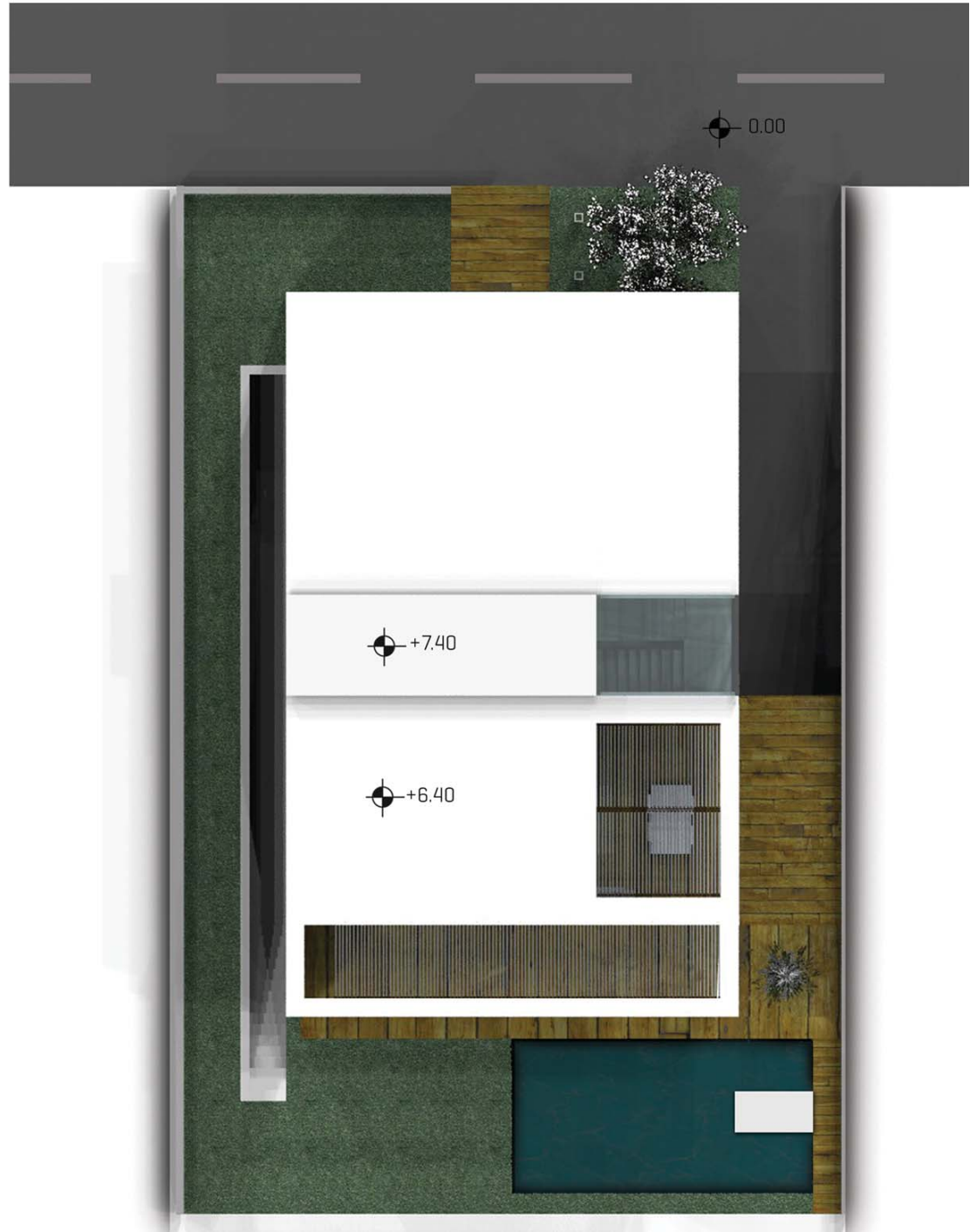


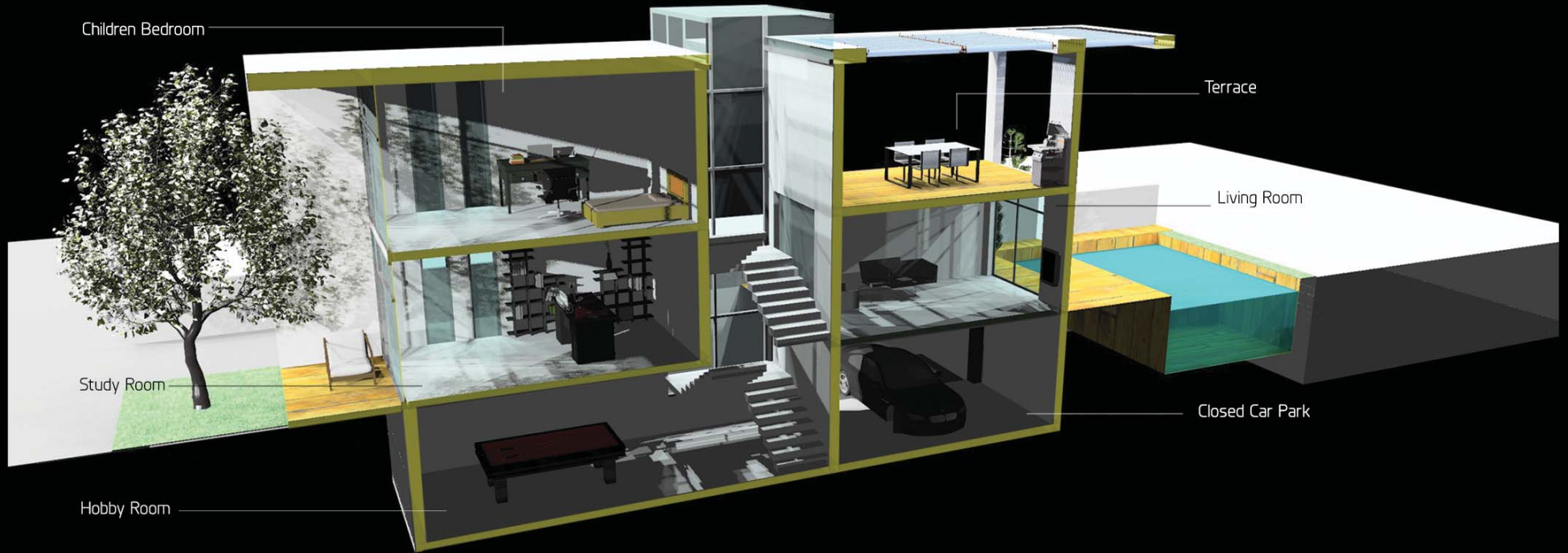
ARCH332 HOUSE Umitköy Floor Plans

+3.00 Floor Plan

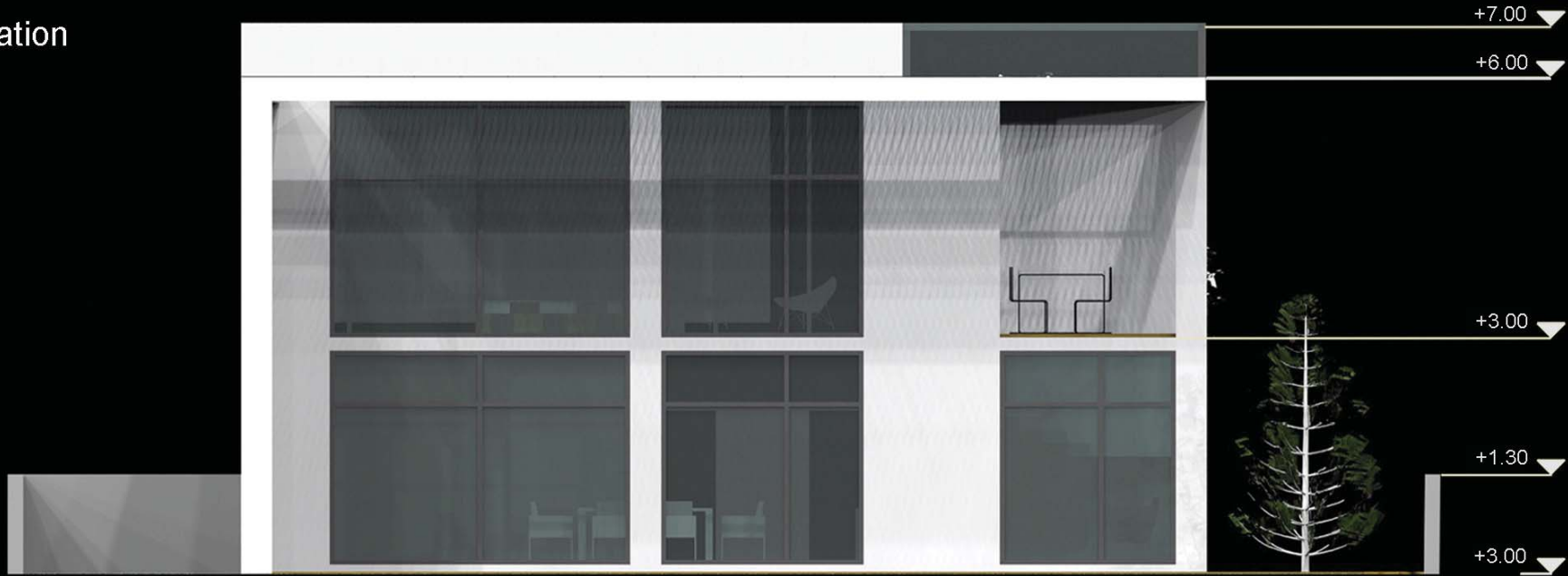


Site Plan





South Elevation



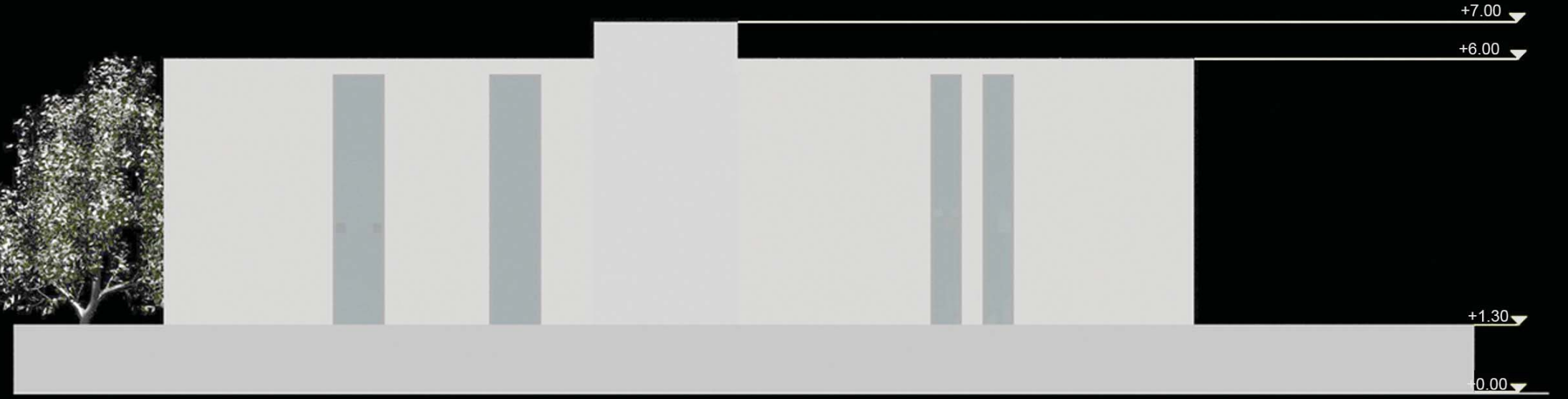
North Elevation

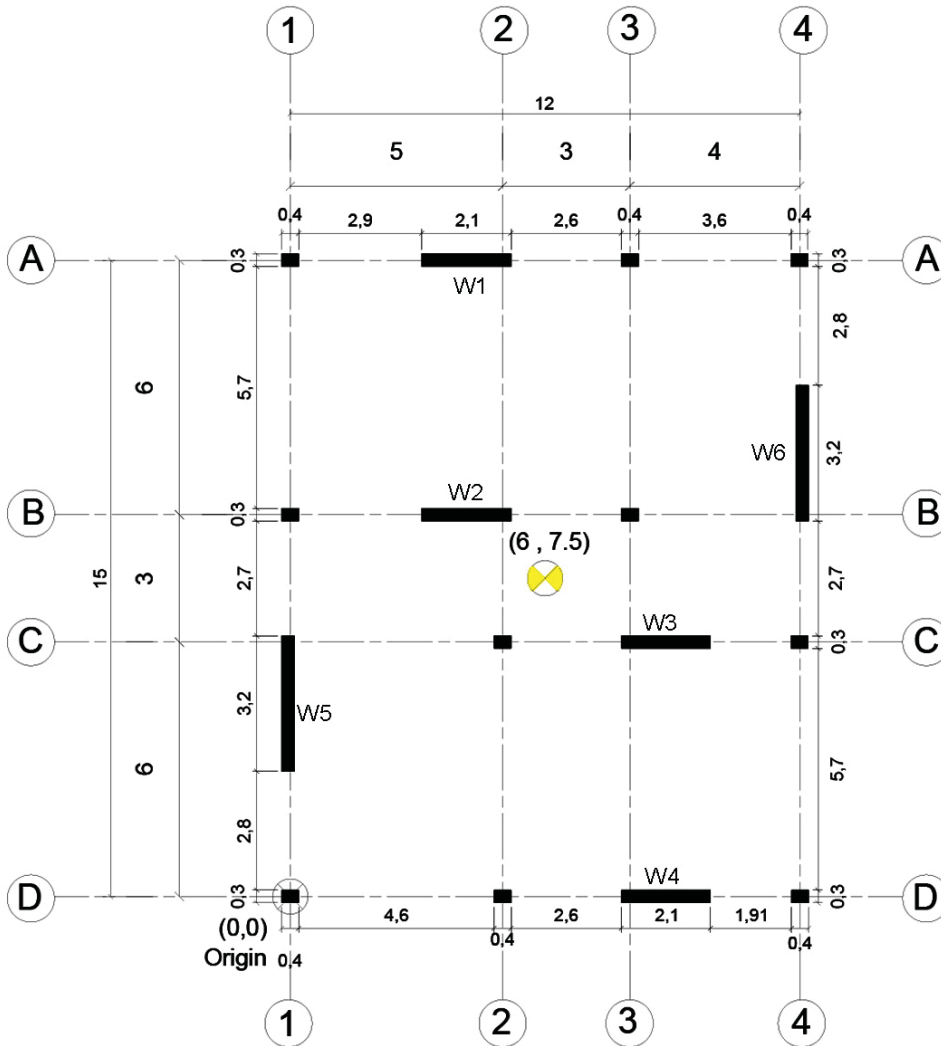


East Elevation



West Elevation





Geometric Center

Since the slab is simply rectangular, the geometric center is located on midpoints of the lengths on X and Y axis. The origin is depicted on the figure.

$$G_x = \frac{12}{2} = 6$$

$$G_y = \frac{15}{2} = 7.5$$

Stiffness Center

Dimensions of shear walls on X axis (namely W5, W4) = 0.3m X 3.2 m

$$X_R = \frac{\frac{1}{12} \times 0.3 \times (3.2)^3 \times 0 + \left[\frac{1}{12} \times 0.3 \times (3.2)^3 \times 12 \right]}{2 \times \left[\frac{1}{12} \times 0.3 \times (3.2)^3 \right]} = 6$$

Dimensions of shear walls on Y axis (namely W1, W2, W3, W4) = 0.3m X 2.1 m

$$X_R = \frac{\frac{1}{12} \times 0.3 \times (2.1)^3 \times 15 + \left[\frac{1}{12} \times 0.3 \times (2.1)^3 \times 9 \right] + \left[\frac{1}{12} \times 0.3 \times (2.1)^3 \times 6 \right] + \left[\frac{1}{12} \times 0.3 \times (2.1)^3 \times 0 \right]}{4 \times \left[\frac{1}{12} \times 0.3 \times (2.1)^3 \right]} = 7.5$$

Shear Wall Percentage

Area of the Footprint of Shear Walls on X Axis
 Floor Area

Total Floor Area : 180 m²

Area of shear walls on Y direction : 0.3 x 2.1 x 4 = 2.52 m²

The ratio of shear wall area on Y direction to floor area : 2.52 / 180 = 0.014 → % 1,4



Area of shear walls on X direction : 0.3 x 3.2 x 2 = 1.92 m²

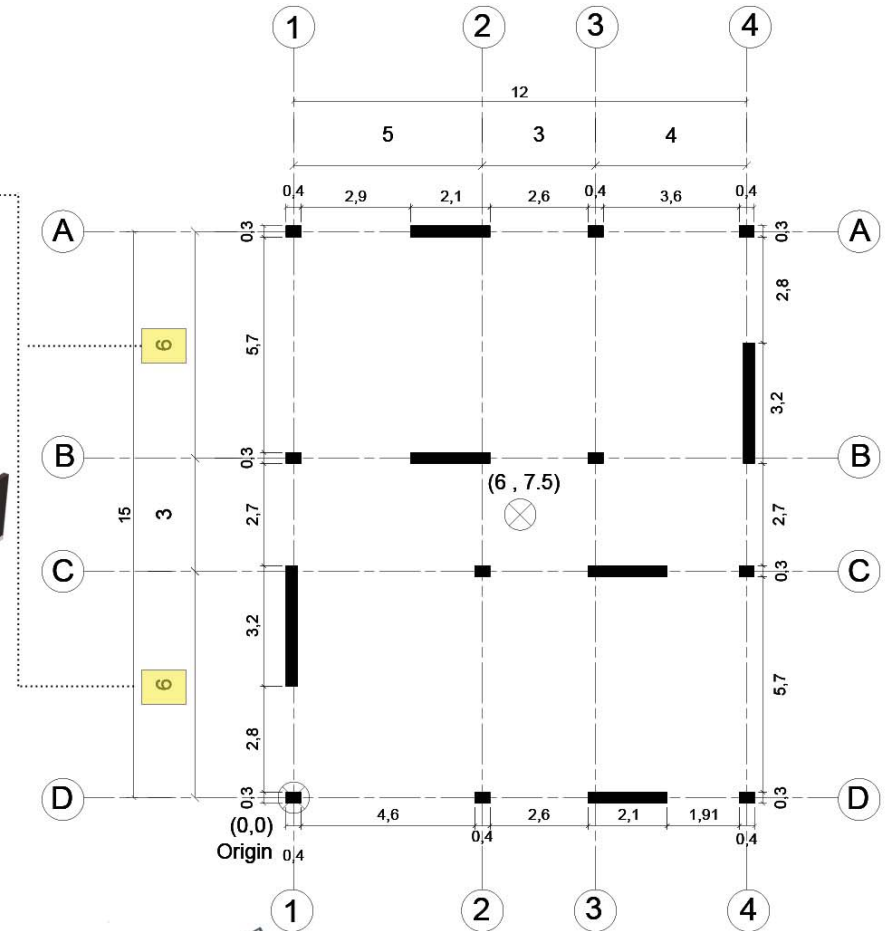
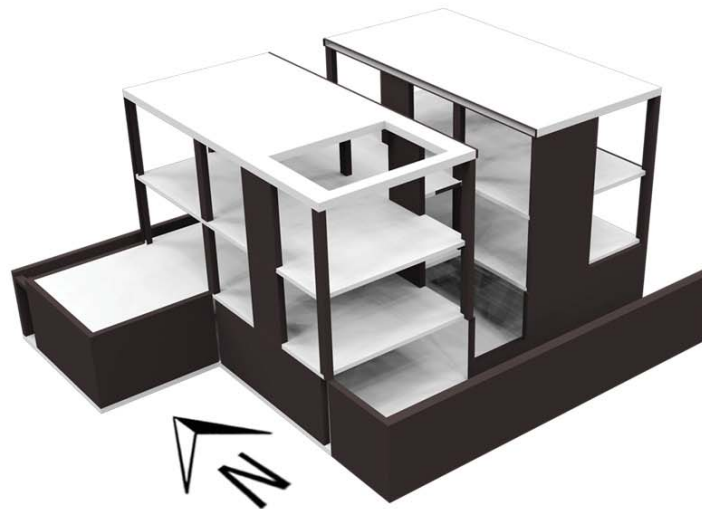
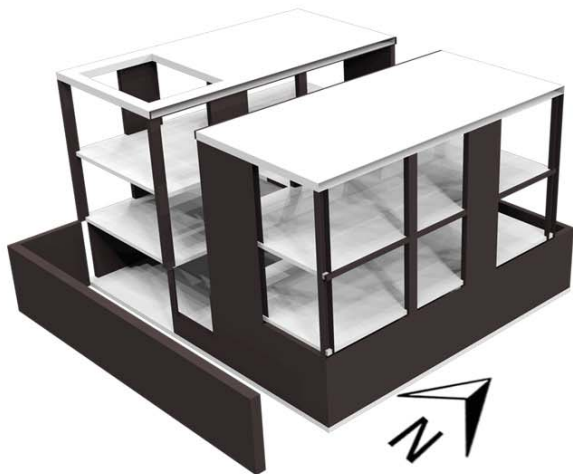
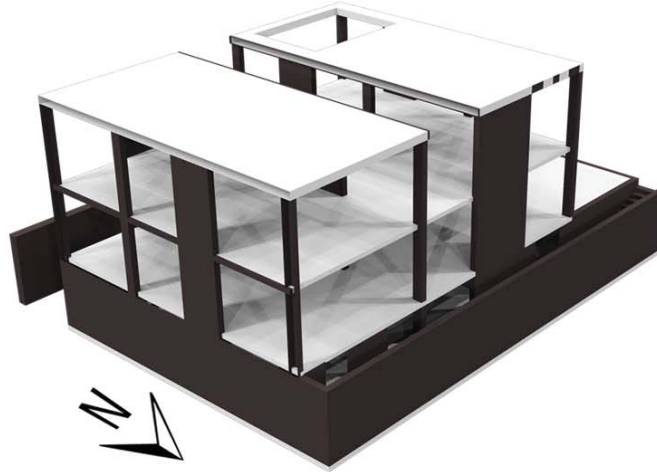
The ratio of shear wall area on X direction to floor area : 1.92 / 180 = 0.0106 → % 1

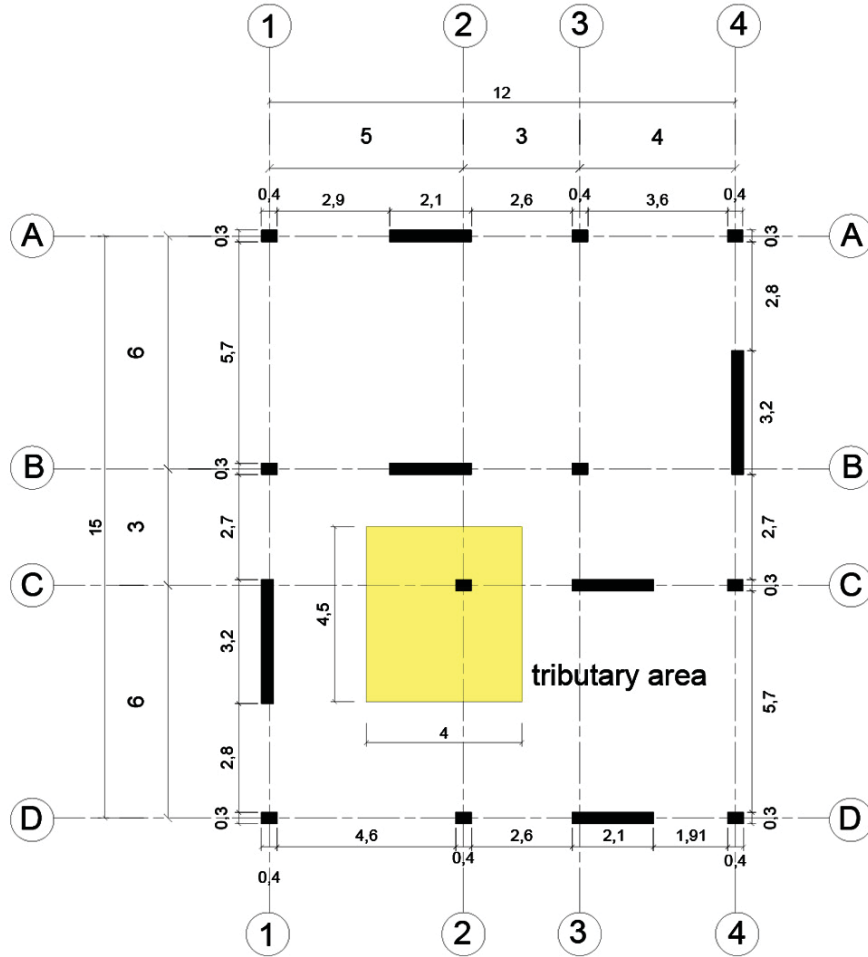


ARCH332 HOUSE Umitköy Slab System

Flat Plate is selected as the structural system. According to the standards
 The minimum thickness should be greater than
 $h > 200\text{mm}$
 $h \geq \text{Long length} / 30$
 The dimensions of columns in the span direction should not be less than
 $1/20$ of the span length in that direction nor less than 300mm.

According to the rules
 we choose **20 cm** as slab thickness.





Design Loads (Live Load and Dead Load)

Dead Load for Flat Slab is:

- Own Weight : $0.2 \times 2.4 = 0.48 \text{ t/m}^2$
- Leveling : $0.04 \times 2.4 = 0.096 \text{ t/m}^2$
- Covering : $0.025 \times 2 = 0.05 \text{ t/m}^2$
- Plastering : $0.02 \times 2 = 0.04 \text{ t/m}^2$

+
 $0.666 \text{ t/m}^2 \sim 0.7 \text{ t/m}^2$

Live Load

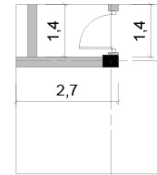
We can consider 200 kg/m^2 (0.2 t/m^2) which is for residential buildings according to the standards.

Total Load = $(1.4 \times \text{DL}) + (1.6 \times \text{LL})$
 $= (1.4 \times 0.7) + (1.6 \times 0.2)$
 $= 1.3 \text{ t/m}^2$

Wall Load

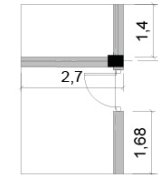
Tributary Area : $4.5 \times 4 = 18 \text{ m}^2$

+0.00 Floor Tributary Area



Total Wall Length : 5.5 m

+3.00 Floor Tributary Area

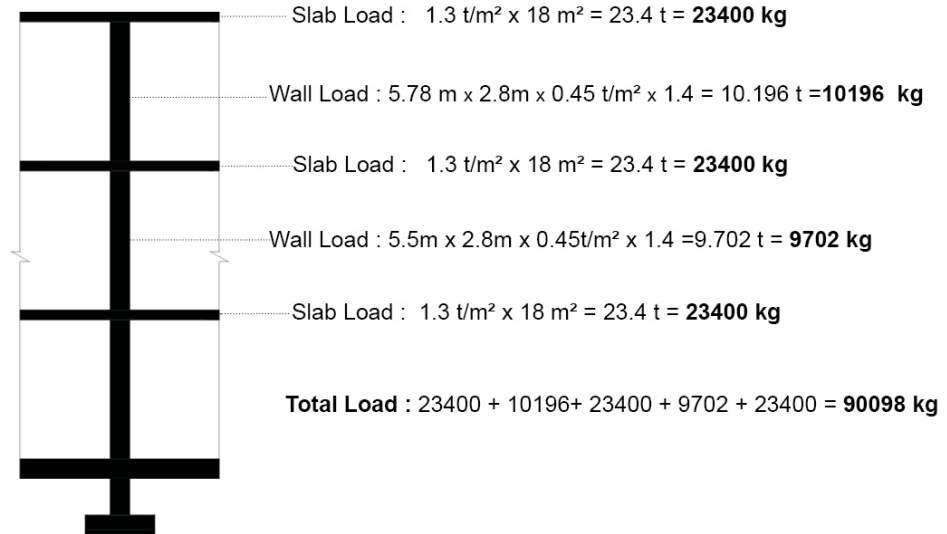


Total Wall Length : 5.78 m

*In order to be on the safe side, door loads are taken as wall loads.

Wall Load = Wall Length x Wall Height x Distributed Wall Load (0.45 t/m^2) x Dead Load Factor
 Slab Load = Total Design Load x Tributary Area

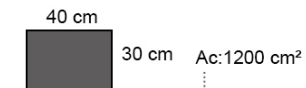
Assume Slab depth is 20 cm and wall height is 280 cm



According to Standards;

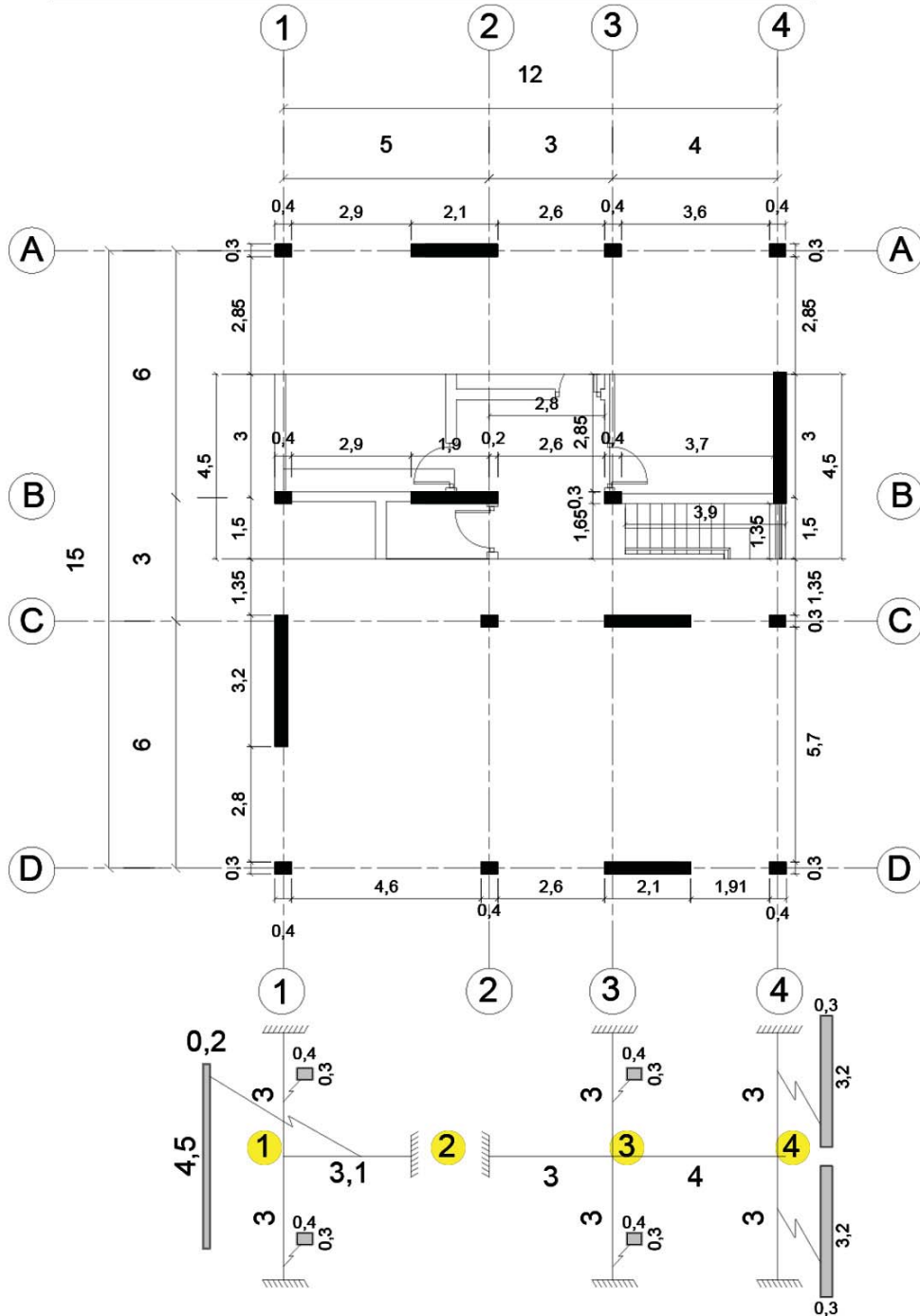
$A_c \geq \frac{N_d}{0.75 \times f_{cd}} = \frac{90098}{0.75 \times 130} = 924 \text{ cm}^2$

$A_c \geq 750 \text{ mm}^2$



According to TS-500 column dimensions : Then; $1200 \text{ cm}^2 > 924 \text{ cm}^2$





The area depicted in the figure chosen for the two cycle method since the columns and the shear walls in that axis have the greatest distance to the other walls and shear walls. We will make the calculation according to the first floor in that area because wall load on the first floor is greater than ground floor. (Live load and the slab load is the same.)

Calculation of Wall Loads (First Floor)

For two cycle graphics, axis 1-2 will be taken as 2.9 m instead of 4.15m but, to be on the safe side, whole wall load on the 1-2 axis was taken (in 4.15 distance).

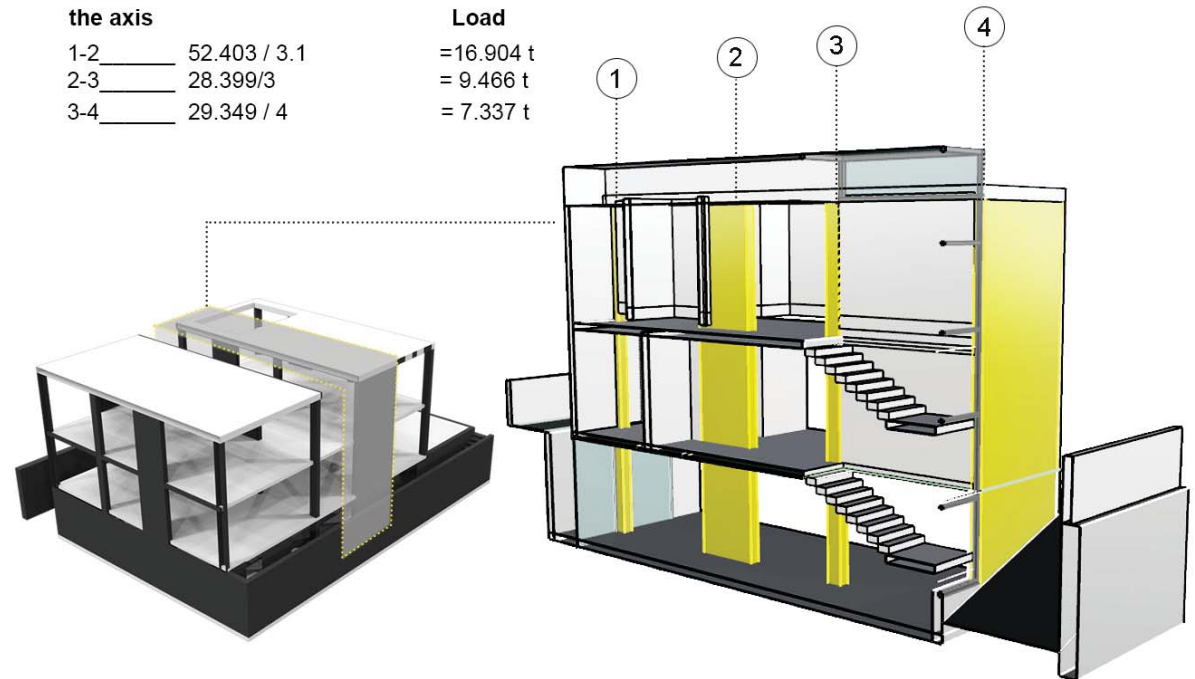
Between the axis	Load	Total Load
1-2	$13.125 \times 2.8 \times 0.45 \times 1.4 = 23.153 \text{ t}$	$23.153 + 29.25 = 52.403 \text{ t}$
2-3	$6.15 \times 2.8 \times 0.45 \times 1.4 = 10.849 \text{ t}$	$10.849 + 17.55 = 28.399 \text{ t}$
3-4	$7.25 \times 2.8 \times 0.45 \times 1.4 = 12.789 \text{ t}$	$12.789 + 16.56 = 29.349 \text{ t}$

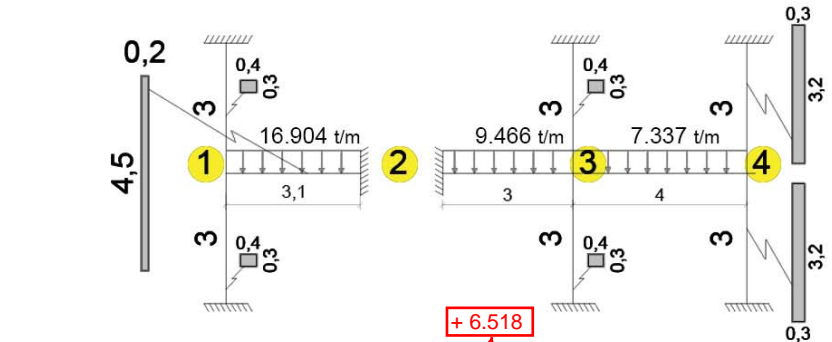
Calculation of Slab Loads (First Floor)

Between the axis	Load
1-2	$1.3 \times 4.5 \times 5 = 29.25 \text{ t}$
2-3	$1.3 \times 4.5 \times 3 = 17.55 \text{ t}$
3-4	$1.3 \times [(4.5 \times 4) - (3.9 \times 1.35)] = 16.56 \text{ t}$ Stair

Calculation of the Distributed Loads (First Floor)

Between the axis	Load
1-2	$52.403 / 3.1 = 16.904 \text{ t}$
2-3	$28.399 / 3 = 9.466 \text{ t}$
3-4	$29.349 / 4 = 7.337 \text{ t}$



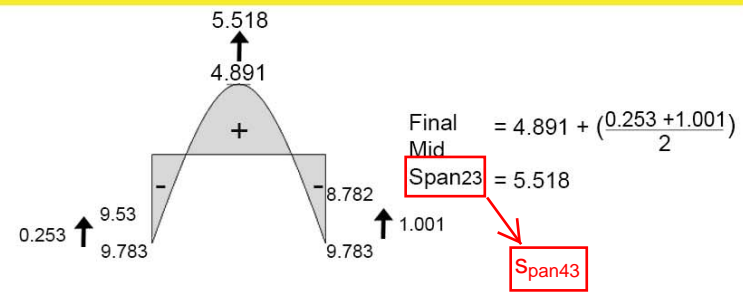
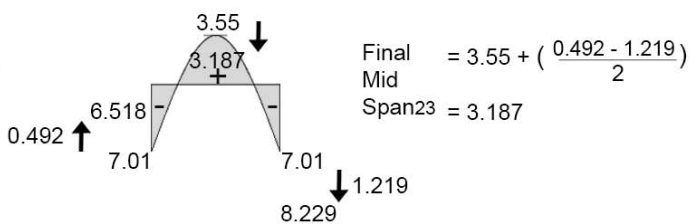
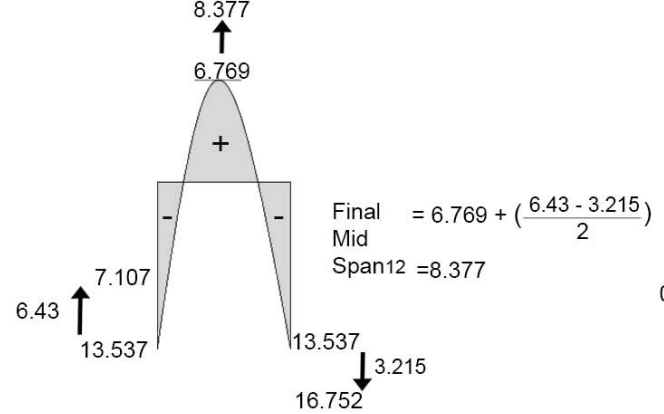
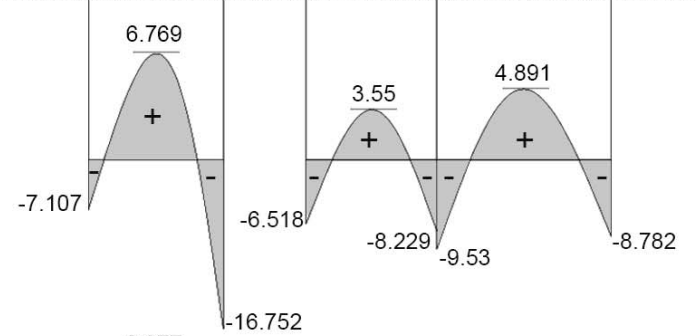


r	0.475	0	0	0.355	0.266	0.135
FEM	13.537	-13.537	7.01	-7.01	9.783	-9.783
1st cycle	0	-3.215	-0.492	0	0.660	-0.369
Σ	13.537	-16.752	-6.518	-7.01	10.443	-10.152
2nd cycle	-6.430	0	0	-1.219	-0.913	1.370
Σ	7.107	-16.752	-6.518	-8.229	9.53	-8.782

$$M.S._{12} = \frac{16.904 \times 3.1^2}{24} = 6.769$$

$$M.S._{23} = \frac{9.466 \times 3^2}{24} = 3.55$$

$$M.S._{34} = \frac{7.337 \times 4^2}{24} = 4.891$$



Calculation of I Values

$$I = \frac{1}{12} \times A \times B^3$$

(flat slab) $I_{12} = I_{23} = I_{34} = \frac{1}{12} \times 4.5 \times (0.2)^3 = 0.003 \text{ m}^4$

(Columns) $I_1 = I_3 = \frac{1}{12} \times 0.3 \times (0.4)^3 = 0.0016 \text{ m}^4$

(Shear Wall) $I_4 = \frac{1}{12} \times 3.2 \times (0.3)^3 = 0.0072 \text{ m}^4$

Calculation of r Values

$$r_{12} = \frac{I_{12}}{L_{12}} = \frac{0.003}{3.1} = 0.475$$

$$r_{21} = 0$$

$$r_{32} = \frac{I_{32}}{L_{32}} = \frac{0.003}{3} = 0.355$$

$$r_{23} = 0$$

$$r_{34} = \frac{I_{34}}{L_{34}} = \frac{0.003}{4} = 0.266$$

$$r_{43} = \frac{I_{43}}{L_{43}} = \frac{0.003}{4} = 0.135$$

$$r_{12} = \frac{I_{12}}{L_{12} + 2 \times \left(\frac{I_1}{L_1}\right)} = \frac{0.003}{3.1 + [2 \times \left(\frac{0.0016}{3}\right)]} = 0.475$$

$$r_{32} = \frac{I_{32} + I_{34} + [2 \times \left(\frac{I_3}{L_3}\right)]}{\frac{I_{32}}{L_{32}} + \frac{I_{34}}{L_{34}} + [2 \times \left(\frac{I_3}{L_3}\right)]} = \frac{0.003 + 0.003 + [2 \times \left(\frac{0.0016}{3}\right)]}{\frac{0.003}{3} + \frac{0.003}{4} + [2 \times \left(\frac{0.0016}{3}\right)]} = 0.355$$

$$r_{43} = \frac{I_{43}}{L_{43} + 2 \times \left(\frac{I_4}{L_4}\right)} = \frac{0.003}{4 + [2 \times \left(\frac{0.0072}{3}\right)]} = 0.135$$

FEM

$$FEM = \frac{q \times l^2}{12}$$

$$FEM_{12} = \frac{16.904 \times (3.1)^2}{12} = 13.537 \text{ tm}$$

$$FEM_{23} = \frac{9.466 \times (3)^2}{12} = 7.01 \text{ tm}$$

$$FEM_{34} = \frac{7.337 \times (4)^2}{12} = 9.783 \text{ tm}$$

Slab Depth

$$K_0 = \frac{b_w \times d^2}{M_{max}}$$

$$0.025 = \frac{450 \times d^2}{1675200} = 9.647$$

Since 20 cm ≥ 9.647cm, our flat is SAFE