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> # Prof. Dr. Serkan Dağ
# ME 451 Introduction to Composite Structures
> # File 7.4.3
# Example on design of a laminate
> restart :
with(LinearAlgebra) :
Digits := 16 :
> # Enter the number of plies
> n := 1 :
> # Define extensional, coupling, and bending stiffness matrices
> A := Matrix(3) :
B := Matrix(3) :
Dm := Matrix(3) :
> # Define laminate stiffness matrix
> QL := Matrix(6) :
> # Define ply surface coordinate vector in inches

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$$h := \begin{bmatrix} -\frac{h_0}{2} \\ 0 \\ \frac{h_0}{2} \end{bmatrix} \quad h := \begin{bmatrix} -\frac{1}{2} h_0 \\ 0 \\ \frac{1}{2} h_0 \end{bmatrix} \quad (1)$$

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> # Define ply angle vector in radians
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$$\theta := [0] \quad (2)$$

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> # Define Qbar array
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Qbar := Array(1..3, 1..3, 1..n) :
ArrayNumElems(Qbar);
```

9

(3)

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> # Enter properties of the unidirectional lamina
# From Table 2.2 for graphite/epoxy (unit = Msi)
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> EI := 26.25 :
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E2 := 1.49 :
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nul2 := 0.28 :
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G12 := 1.040 :
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> # Calculate elements of the compliance matrix for the
unidirectional lamina
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> S11 :=  $\frac{1}{EI}$  :
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S12 := - $\frac{nul2}{EI}$  :
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S22 :=  $\frac{1}{E2}$  :
S66 :=  $\frac{1}{G12}$  :
> # Calculate elements of the reduced stiffness matrix for the
  unidirectional lamina
> Q11 :=  $\frac{S22}{S11 \cdot S22 - S12^2}$  :
Q22 :=  $\frac{S11}{S11 \cdot S22 - S12^2}$  :
Q12 := - $\frac{S12}{S11 \cdot S22 - S12^2}$  :
Q66 :=  $\frac{1}{S66}$  :
> # Calculate elements of transformed reduced stiffness matrix for
  each angle lamina
# Unit = Msi
> for i from 1 by 1 to n
  while true do
    Qbar[1, 1, i] := Q11 · (cos(theta[i, 1]))4 + Q22 · (sin(theta[i, 1]))4 + 2 · (Q12 + 2 · Q66)
      · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2 :
    Qbar[1, 2, i] := (Q11 + Q22 - 4 · Q66) · (sin(theta[i, 1]))2 · (cos(theta[i, 1]))2 + Q12
      · ((cos(theta[i, 1]))4 + (sin(theta[i, 1]))4) :
    Qbar[1, 3, i] := (Q11 - Q12 - 2 · Q66) · (sin(theta[i, 1])) · (cos(theta[i, 1]))3 - (Q22 - Q12
      - 2 · Q66) · (sin(theta[i, 1]))3 · cos(theta[i, 1]) :
    Qbar[2, 2, i] := Q11 · (sin(theta[i, 1]))4 + Q22 · (cos(theta[i, 1]))4 + 2 · (Q12 + 2 · Q66)
      · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2 :
    Qbar[2, 3, i] := (Q11 - Q12 - 2 · Q66) · (cos(theta[i, 1])) · (sin(theta[i, 1]))3 - (Q22 - Q12
      - 2 · Q66) · (cos(theta[i, 1]))3 · sin(theta[i, 1]) :
    Qbar[3, 3, i] := (Q11 + Q22 - 2 · Q12 - 2 · Q66) · (cos(theta[i, 1]))2 · (sin(theta[i, 1]))2
      + Q66 · ((cos(theta[i, 1]))4 + (sin(theta[i, 1]))4) :
    Qbar[2, 1, i] := Qbar[1, 2, i] :
    Qbar[3, 1, i] := Qbar[1, 3, i] :
    Qbar[3, 2, i] := Qbar[2, 3, i] :
  end do:
> # Calculate elements of extensional stiffness matrix [A],
  coupling stiffness matrix [B], and bending stiffness matrix [Dm]
# Units: [A]--> Msi.in; [B]--> Msi.in2; [Dm]--> Msi.in3
> for i from 1 by 1 to 3
  while true do
    for j from 1 by 1 to 3
      while true do
        A[i, j] := 0 :
        B[i, j] := 0 :
        Dm[i, j] := 0 :
        for k from 1 by 1 to n
          while true do

```

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A[i,j] := A[i,j] + Qbar[i,j,k]·(h[k+1,1] - h[k,1]) :
B[i,j] := B[i,j] +  $\frac{1}{2}$ ·Qbar[i,j,k]·(h[k+1,1]2 - h[k,1]2) :
Dm[i,j] := Dm[i,j] +  $\frac{1}{3}$ ·Qbar[i,j,k]·(h[k+1,1]3 - h[k,1]3) :
end do:
end do:
end do:
> evalf( A );

$$\begin{bmatrix} 26.36733817050383 h0 & 0.4190648946565411 h0 & 0. \\ 0.4190648946565411 h0 & 1.496660338059075 h0 & 0. \\ 0. & 0. & 1.040000000000000 h0 \end{bmatrix} \quad (4)$$

> evalf( B );

$$\begin{bmatrix} 0. & 0. & 0. \\ 0. & 0. & 0. \\ 0. & 0. & 0. \end{bmatrix} \quad (5)$$

> evalf( Dm );

$$\begin{bmatrix} 2.197278180875319 h0^3 & 0.03492207455471177 h0^3 & 0. \\ 0.03492207455471177 h0^3 & 0.1247216948382563 h0^3 & 0. \\ 0. & 0. & 0.08666666666666667 h0^3 \end{bmatrix} \quad (6)$$

> # Form laminate stiffness matrix QL
> for i from 1 by 1 to 3
  while true do
    for j from 1 by 1 to 3
      while true do
        QL[i,j] := A[i,j]:
        QL[i,j+3] := B[i,j]:
        QL[i+3,j] := B[i,j]:
        QL[i+3,j+3] := Dm[i,j]:
      end do:
    end do:
> # Form loading vector N
> N := 
$$\begin{bmatrix} 0 \\ 0 \\ 0 \\ 3250 \cdot (10)^{-6} \\ 0 \\ 0 \end{bmatrix};$$


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$$N := \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{13}{4000} \\ 0 \\ 0 \end{bmatrix} \quad (7)$$

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> # Find midplane strains and curvatures
> Res := evalf( LinearSolve(QL, N) );
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$$Res := \begin{bmatrix} 0. \\ 0. \\ 0. \\ \frac{0.001485714285714286}{h\theta^3} \\ -\frac{0.0004160000000000003}{h\theta^3} \\ 0. \end{bmatrix} \quad (8)$$

```
> # Find strains
> eps_x := z*Res[4, 1];
eps_y := z*Res[5, 1];
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$$\begin{aligned} \text{eps}_x &:= \frac{0.001485714285714286 z}{h\theta^3} \\ \text{eps}_y &:= -\frac{0.0004160000000000003 z}{h\theta^3} \end{aligned} \quad (9)$$

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> # Find stresses
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$$\begin{aligned} \sigma_x &:= Qbar[1, 1, 1] \cdot \text{eps}_x + Qbar[1, 2, 1] \cdot \text{eps}_y; \\ \sigma_y &:= Qbar[2, 1, 1] \cdot \text{eps}_x + Qbar[2, 2, 1] \cdot \text{eps}_y; \\ \sigma_{xy} &:= Qbar[3, 1, 1] \cdot \text{eps}_x + Qbar[3, 2, 1] \cdot \text{eps}_y; \\ \sigma_x &:= \frac{0.03900000000000001 z}{h\theta^3} \\ \sigma_y &:= -\frac{1.10^{-19} z}{h\theta^3} \\ \sigma_{xy} &:= 0. \end{aligned} \quad (10)$$

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> # Find thickness
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$$h := \sqrt{\left(\frac{3.9e-2}{2} \cdot \frac{1000}{\left(\frac{217.56}{2}\right)}\right)}; \quad (11)$$

$$h := 0.4233921274027279 \quad (11)$$

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> # Find number of plies  
> N :=  $\frac{h}{0.0049213};$   
N := 86.03257826239570  
>
```

$$(12)$$